Competition Between Cavitation and Flow in Amorphous Solids

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postdoc opportunity!

JOHNS HOPKINS

WHITING SCHOOL of ENGINEERING

Bulk Metallic Glasses

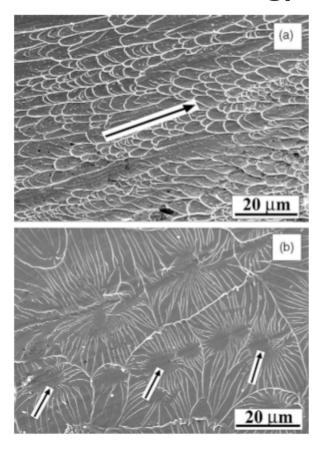


Douglas Hoffman, E-Science News 1998

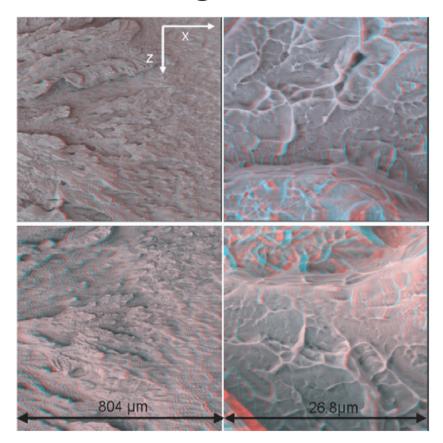
- Unique material with promising properties, but disordered structure.
- What can molecular dynamics simulation tell us about the mechanical response of these materials?

Fracture in Metallic Glass

Phenomenology of fracture in metallic glass



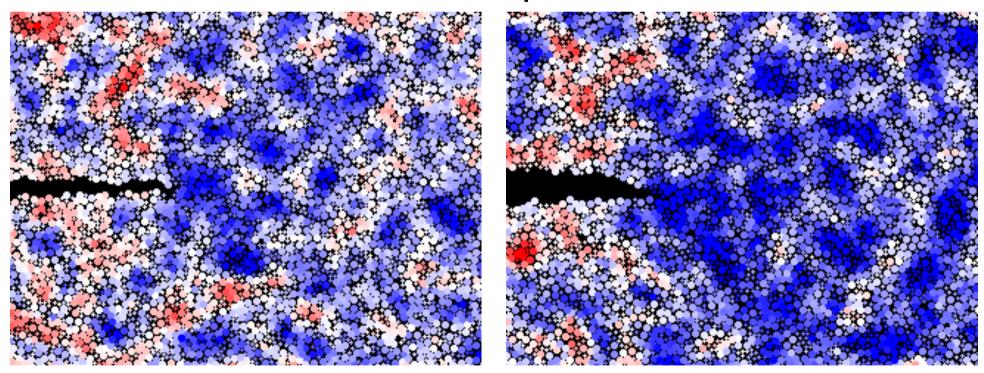
Compressive and Tensile Fracture in Zr₅₉Cu₂₀Al₁₀Ni₈Ti₃
Zhang, Eckert and Schultz
Acta Materialia, 51, pp.1167 (2003)



Tensile fracture in Vitreloy I
Bouchaud, Boivin, Pouchou, Bonamy, Poon and
Ravichandran
Europhysics Letters, V83, pp. 66006 (2008)

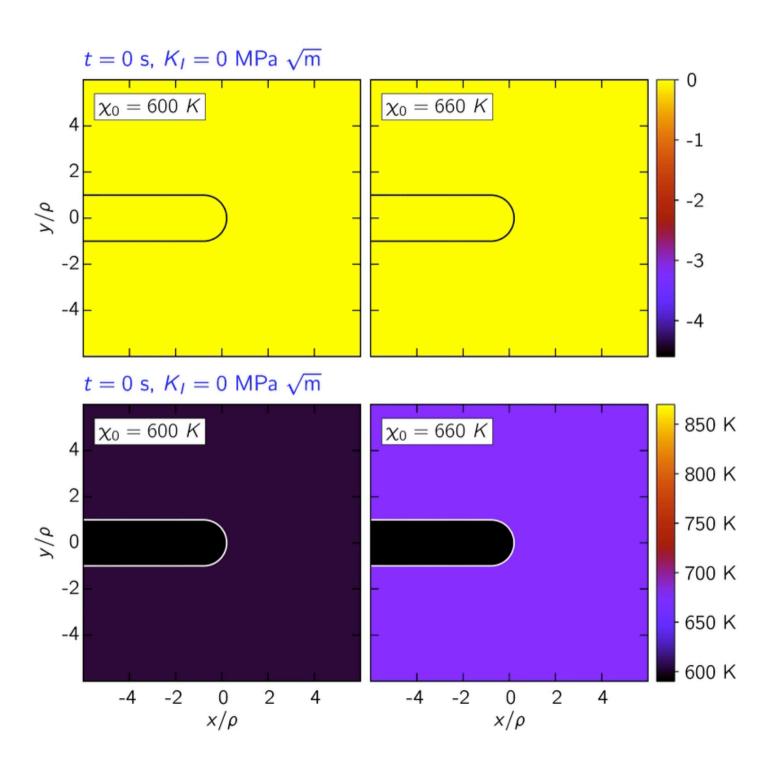
MD Simulations of Fracture

- Simple model of a polydisperse system interacting with pairwise potential
- Both "ductile" and "brittle" simulations exhibit cavitation ahead of crack tip.

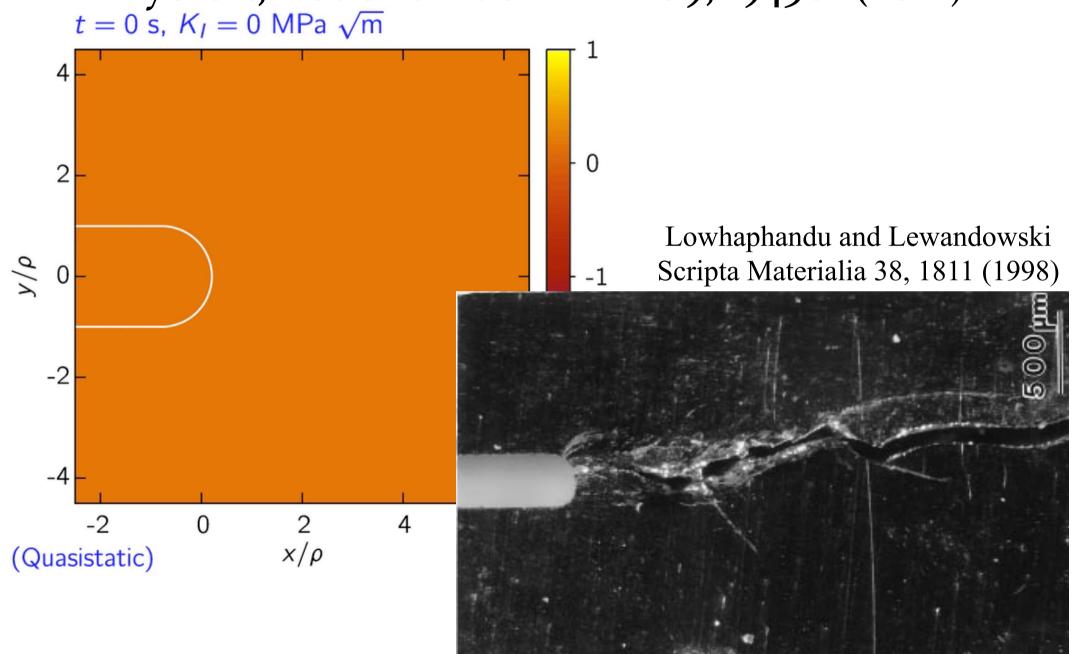


ML Falk, PRB, V60, 7062 (1999)

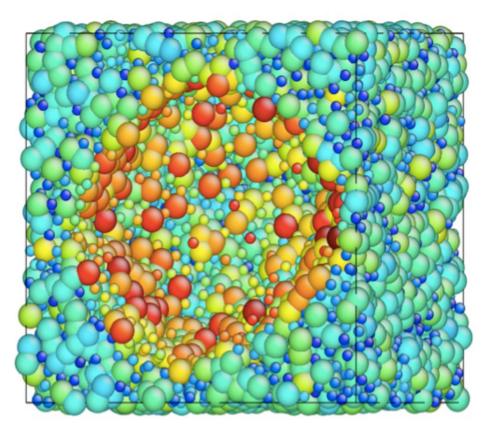
Chris Rycroft, UC Berkeley Urack



Fracture with Cavitation Rycroft, Bouchbinder PRL 109, 194301 (2012)

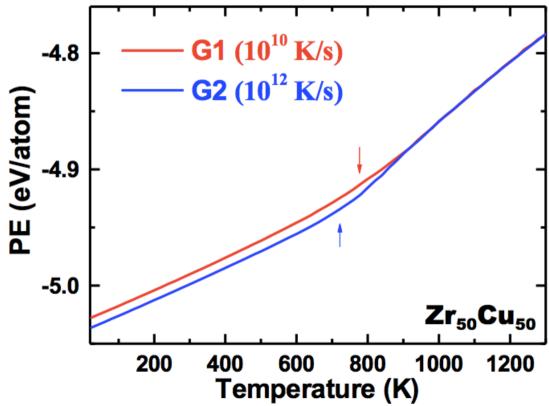


Simulated System: Cu₅₀Zr₅₀

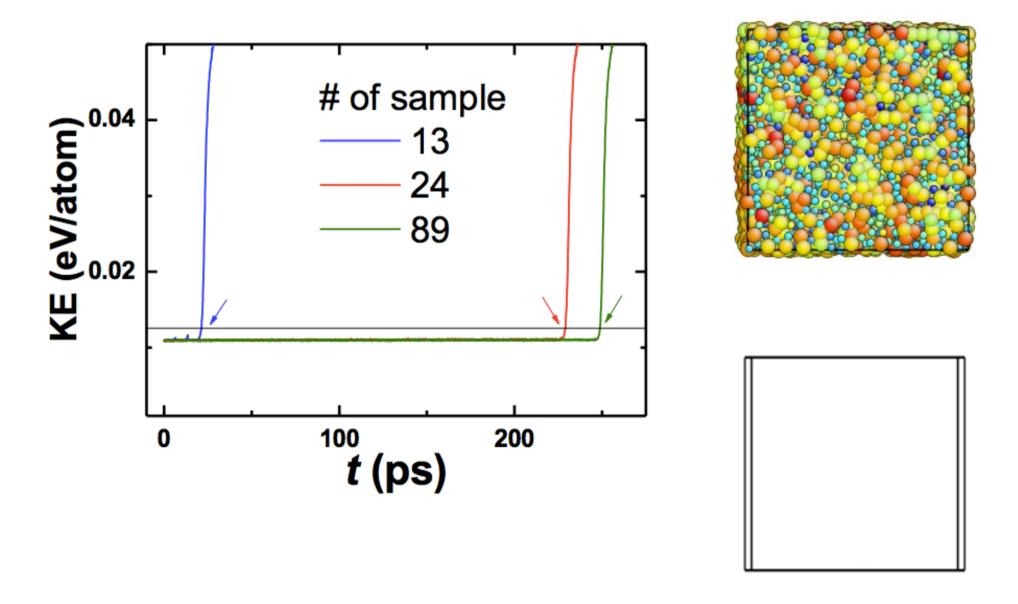


 Unlike crystalline systems, it is not possible to skip simulating the processing step

- EAM Potential
 Y. Q. Cheng and E. Ma, Prog. Mater. Sci. 56, 379 (2011)
- 16,000 atoms
- Quench rates IK/ps and 0.01K/ps



Cavitation At Constant Strain



Homogeneous or Heterogeneous?

- Macroscopically glasses appear isotropic and homogeneous.
- Structurally glasses are in many ways structurally similar to a liquid.
- However, cavitation in structurally identical samples with randomized initial velocities occurs at the same location implying heterogeneous nucleation.
- Use MD to test theories of nucleation.
- Measure the critical cavity size and determine how it compares to the CNT prediction.

Classical Nucleation in Solids

 For a cavity nucleus to be unstable, the incremental elastic energy released must exceed the incremental surface energy and plastic work required to grow.

$$dF_e > dF_s + \delta W_p$$

$$4\pi K \epsilon_{\infty} r^2 dr > 8\pi \gamma r dr + \delta W_p(r, \dot{r})$$

 An estimate of the plastic work depends on assumptions regarding constitutive response, thermal softening and other difficult to ascertain details.

Classical Nucleation in Solids

- We make 3 assumptions:
 - spherical cavity
 - rate independence of plastic work
 - plastic work scales with volume

$$4\pi K \epsilon_{\infty} r^2 dr > 8\pi \gamma r dr + \delta W_p(r, \dot{r})$$

 Under these conditions plastic work can be captured by a single parameter that determines the critical strain below which cavitation is impossible

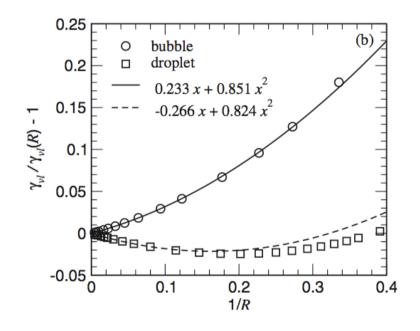
$$4\pi K \left(\epsilon_{\infty} - \epsilon_{c}\right) r^{2} dr > 8\pi \gamma r dr$$

Radius Dependence of Surface Energy "Tolman Length"

 It is known that for small nuclei (bubbles) the surface energy varies with bubble size

$$\gamma = \frac{\gamma_{\infty}}{1 + \frac{2\delta}{r}}$$

For work on Tolman length in liquid see An, Garrett, Samwer, Liu, Zybin, Luo, Johnson, Goddard, Journal of Physical Chemistry Letters, 2, 1320-1323 (2011)



Block, Das, Oettel, Viranu and Binder, Curvature dependence of surface free energy of liquid drops and bubbles: A simulation study, ICP, 133, 154702 (2010)

Classical Nucleation in Solids

$$\gamma = \frac{\gamma_{\infty}}{1 + \frac{2\delta}{r}}$$

We can infer a critical cavity size

$$r^* = \frac{2\gamma_{\infty}}{K(\varepsilon - \varepsilon_c)} \qquad r_c = r^* \left(\frac{1}{2} + \frac{1}{2} \sqrt{1 + \frac{4\delta}{r^*}} - \frac{2\delta}{r^*} \right)$$

 And a critical free energy fluctuation for nucleation

$$F_c \equiv 4\pi \gamma r_c^2 - \frac{4}{3}\pi K(\epsilon_{\infty} - \epsilon_c)r_c^3$$

Parameters in Theory

$$R = f \exp\left(-\frac{F_c}{k_B T}\right) r^* = \frac{2\gamma_{\infty}}{K(\varepsilon - \varepsilon_c)} r_c = r^* \left(\frac{1}{2} + \frac{1}{2}\sqrt{1 + \frac{4\delta}{r^*}} - \frac{2\delta}{r^*}\right)$$

- Independent variables
- Directly measurable parameters

- From T scaling
- From dKE/d(PV) during expansion
- Tolman Length is fitted

$$k_BT, \epsilon_{\infty}$$

$$\gamma_{\infty}$$
=0.080 eV/Å²

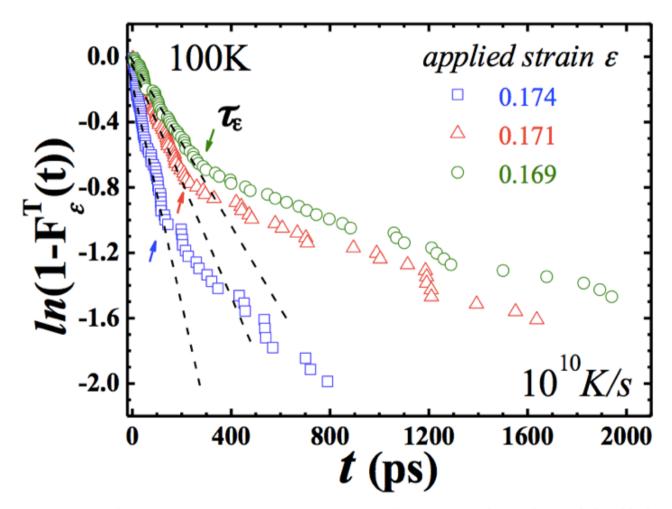
$$f = 0.1ps^{-1}$$

$$\varepsilon_c = 0.02$$

$$\delta=1.15$$
Å

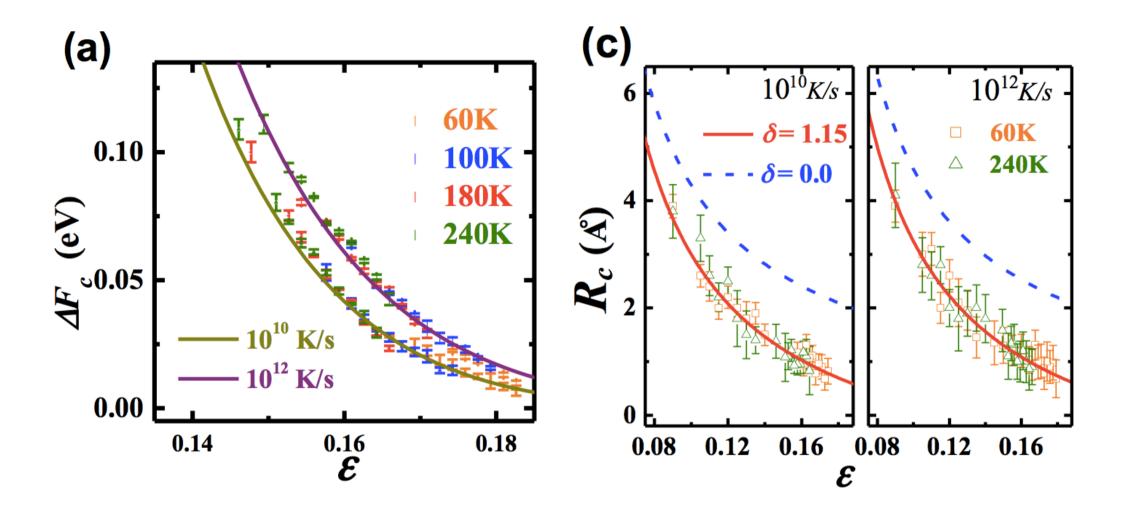
Cavitation: Strain and Hold

Log of fraction of samples not yet cavitated at a given time for a given applied remote strain.

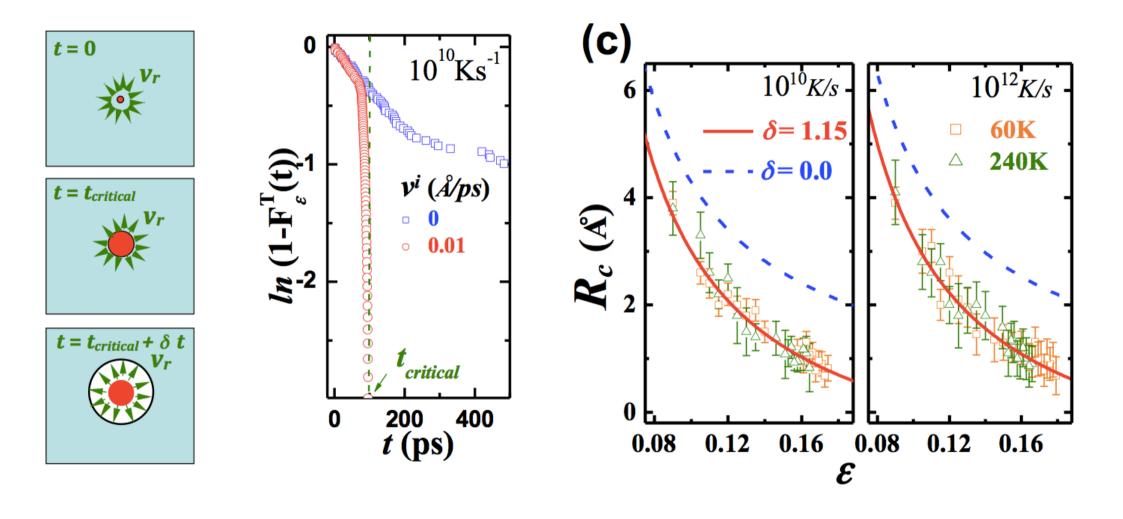


Guan, Lu, Spector, Valavala, Falk, PRL 110, 185502 (2013)

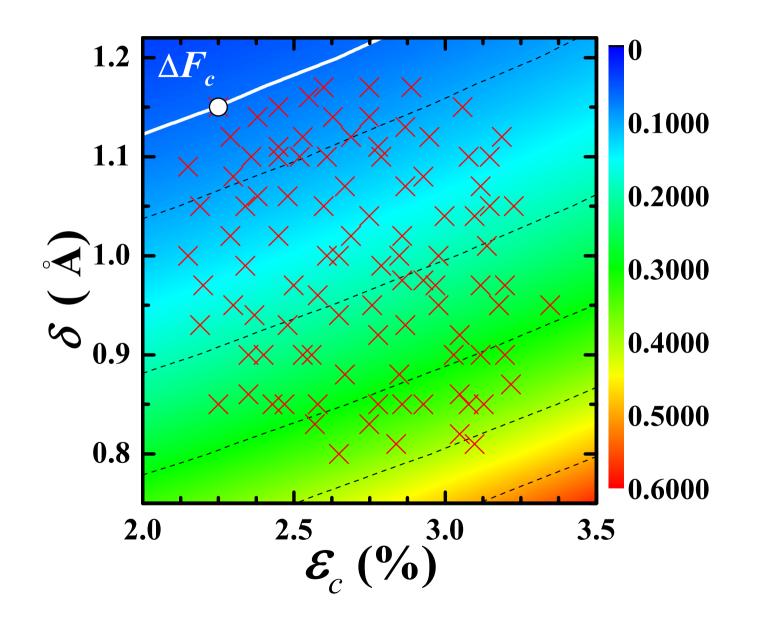
Theory vs. Simulation: Prior to Aging



Theory vs. Simulation: Prior to Aging

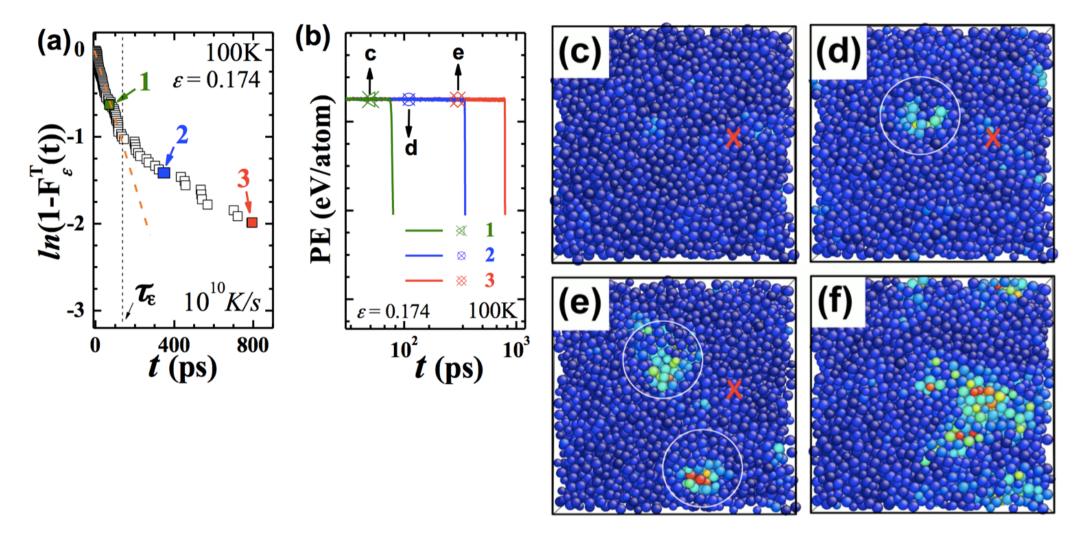


Nature of Local Fluctuations

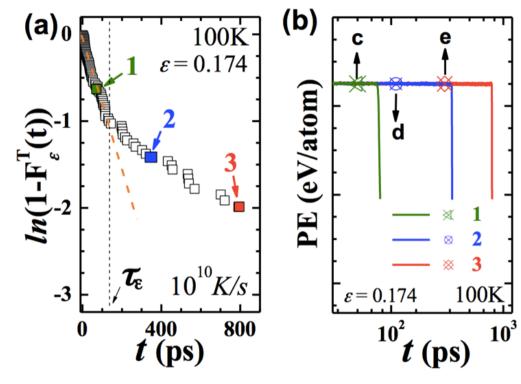


- Low
 correlation
 between
 Tolman length
 and critical
 strain (<0.13)
- 3.4 times
 more sensitive
 to Tolman
 length than
 critical strain.

Onset of Aging: STZ activity

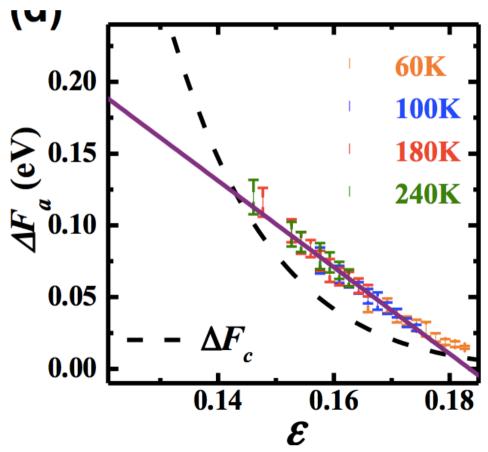


Onset of Aging: STZ activity



- Measured activation volume: 4.5Å³
- Extrapolated zero strain activation energy: 0.55eV

$$R_a = f_a \exp\left(\frac{-\Delta F_a}{k_B T}\right)$$



Conclusions

- Cavitation may play a crucial role in the fracture process zone.
- Plastic dissipation suppresses cavitation at low strains.
- Barrier to cavitation is reduced due to "Tolman Length" effects that decrease surface energy at small radii.
- At short time scales Poissonian rate is predicted by CNT.
- The critical radius under hight tensile strain 14%-18% is very small (1Å-4Å) as confirmed by comparison to simulation.
- Spatial fluctuations in surface energy and, to a lesser degree, susceptibility to plasticity result in heterogeneous nucleation.
- Aging coincides with STZ activity for which we extract an activation barrier and activation volume.
- STZ activation is favored over cavitation at low strains.
- Acknowldegement: NSF DMR 0808704 and 1107838